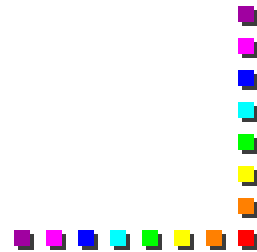


Grating Spectrometers: Echelle Gratings

Astronomy 525

Lecture 09



Outline

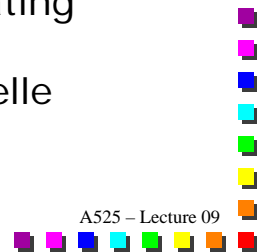
Echelle Spectrometers

- Free spectral range
- Echelle Efficiencies
- Design Parameters
- Example: GEDI – near IR planet finder
- More examples (not covered in class)
 - KEGS – a mid-IR echelle grating spectrometer
 - ZEUS – a submillimeter echelle grating spectrometer

Echelle Gratings

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Echelle Gratings

- An echelle grating is a grating that is coarsely ruled, so that the distance between rulings is greater than the wavelength of interest. It is used at large angles of incidence, and refraction.
- Recall the expression for the (slit limited) resolving power of a grating:

$$R_s = 2 \cdot \tan \alpha \cdot G_{\text{proj}} / \{\theta_{\text{Beam}} \cdot D_{\text{Tel}}\}$$

- For an echelle in Littrow mode, $\alpha, \beta = 63.5^\circ \Rightarrow \tan \alpha = 2$
(This is called an **R2 echelle**, since $\tan \alpha = 2$, For a first order grating, typically $\tan \alpha = 1/2$)
- Therefore, for a given collimated beam size, an echelle spectrometer delivers a higher resolving power. It can also cover a broad range of wavelengths.

Echelle Gratings

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Free Spectral Range: I

- If a grating is operated in echelle mode, resonating at wavelength λ in order n , then it will also resonate at the same angle at another wavelength, λ' in an order $n+1$ where the relationship between orders and wavelengths is given by:

$$n\lambda = d \cdot (\sin \alpha + \sin \beta) = (n+1)\lambda'$$

α (β) = incidence
(diffracted) angle
w.r.t grating
normal

- The difference between these two resonant wavelengths is:

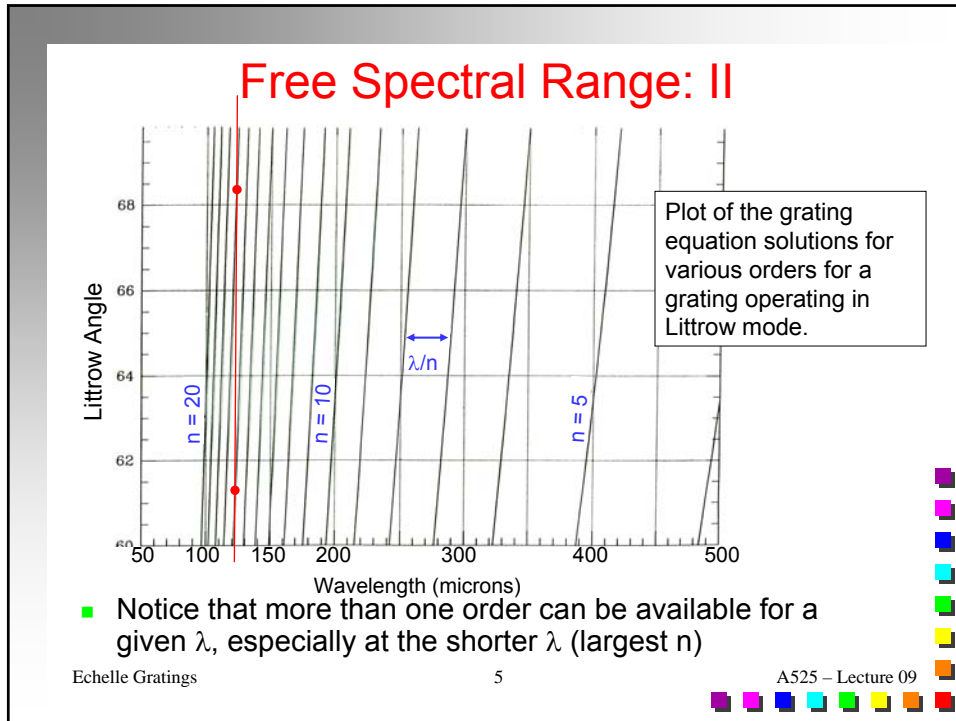
$$\Delta\lambda = \lambda - \lambda' = \lambda' / n$$

- $\Delta\lambda$ is called the **free spectral range**, and is the wavelength interval covered by one order in the echelle without aliasing
- Notice the simple relationship $n\lambda = (n+1)\lambda'$, which is quite useful for quick analysis.

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Echelle Efficiency: I

- It is very important to find the efficiency of diffraction over the various wavelengths in a given free spectral range.
- Recall:

$$I = I_0 \{ \sin(N\gamma) / N \sin(\gamma) \}^2 \cdot \{ \sin(\gamma') / (\gamma') \}^2$$

$$\propto \text{IF} \cdot \text{BF}$$

← Blaze Function
← Interference Function

where:

$$\gamma = \pi d / \lambda \cdot (\sin\beta + \sin\alpha) \quad d = \text{space between slits}$$

$$\gamma' = \pi b / \lambda \cdot (\sin\beta + \sin\alpha) \quad b = \text{width of slit}$$

- The IF is a maximum at $\gamma = m\pi$ (as before), and $\text{IF}_{\text{max}} = 1$
- The BF is a single slit diffraction pattern, with a maximum at $\gamma' = 0$ ($n = 0$ in the grating equation)

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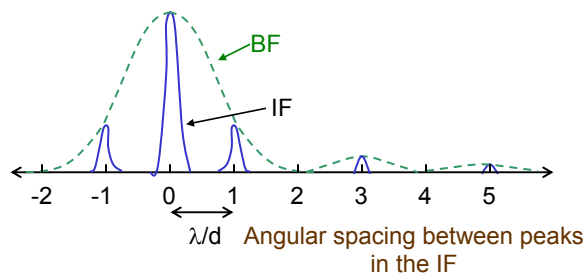
Echelle Efficiency: II

- We saw before that in order to increase the efficiency in a dispersed order ($n \neq 0$), it is necessary to tilt the facets by an angle ϕ (*blazing*, recall that ϕ is the angle of the facet normal w.r.t. the grating normal), so that:

$$\gamma' = \pi b \cos \phi / \lambda \cdot [\sin(\beta - \phi) + \sin(\alpha - \phi)]$$

- The maximum in the BF occurs for:

$$\gamma' = 0 \Rightarrow \alpha + \beta = 2\phi \quad (\text{Blaze } \lambda)$$

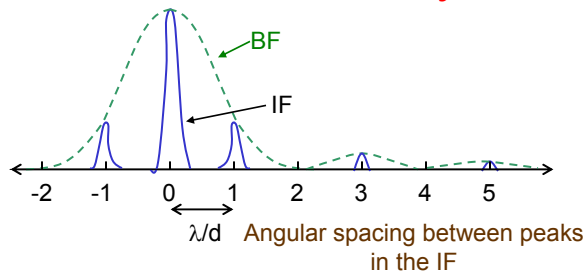


Echelle Gratings

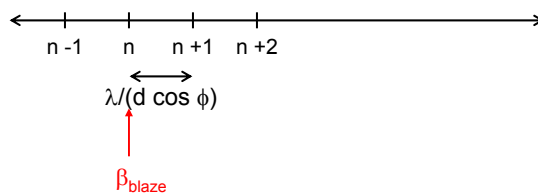
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Echelle Efficiency: III



- Blazing shifts the BF by n orders:



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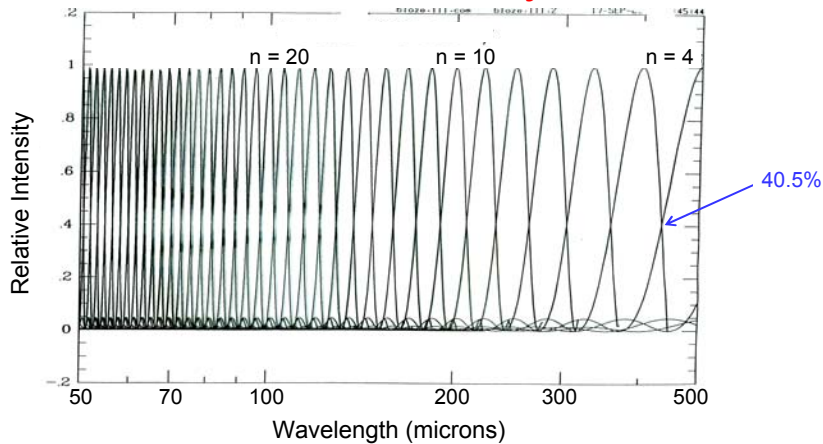
Which order to use?

- We wish to evaluate the BF at the $n + 1$, and $n - 1$ orders.
One can show:
for $\Delta\beta = \lambda/(d \cos \phi)$: $BF = 0.405$ (from the BF) (1)
- From the Grating Equation: $n\lambda = d \cdot (\sin\alpha + \sin\beta)$
 $\Rightarrow n \Delta\lambda/d = \cos\beta \Delta\beta$ (2)
- Combining equations (1) and (2) we have:
 $n \Delta\lambda/d = \lambda/(d \cos \phi) \cdot \cos\beta$
- Littrow mode ($\phi = \alpha = \beta$) $\Rightarrow \Delta\lambda = \lambda/n$, which we identify as the free spectral range. Therefore, the efficiency at the edges of the free spectral range are about 40% in the blaze function.

Conclusion: *We ought to change orders when we observe a wavelength near the edge of the FSR.*



Echelle Efficiency - V



- Relative intensity (efficiency) as a function of λ for various orders, n
- Notice how the orders cross at 40.5% efficiency



Cross Dispersion

- Different orders of the echelle can be separated with a predisperser, such as a grating, prism, or grism.
- The number of orders required is determined by:

$$n_{st} \lambda_2 = (n_{st} + m) \lambda_1$$

$$\Rightarrow m = \frac{\lambda_2 - \lambda_1}{\lambda_1} n_{st}$$

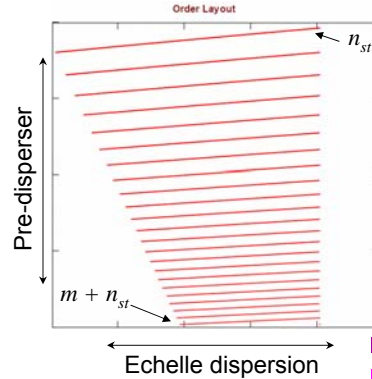
n_{st} = starting order
 m = # of orders

- The starting order can be shown to be:

$$n_{st} = \frac{P_{samp}}{N_{pe}} R$$

P_{samp} = samples/ $\Delta\lambda_R$
 N_{pe} = # pix in echelle direction

$$\Delta\lambda_{FSR} = \frac{\lambda}{n} ; \Delta\lambda_R = \frac{\lambda}{R} ; \frac{N_{pe}}{P_{samp}} = \frac{\Delta\lambda_{FSR}}{\Delta\lambda_R} \Rightarrow n = \frac{P_{samp}}{N_{pe}} R$$



Echelle Gratings

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Gap Between Orders

- Of importance is the smallest gap between orders which occurs at the shortest wavelength
- For a 1st order grating pre-disperser, at the shortest wavelength :

$$\lambda_1 = d_g (\sin \alpha_g + \sin \beta_1)$$

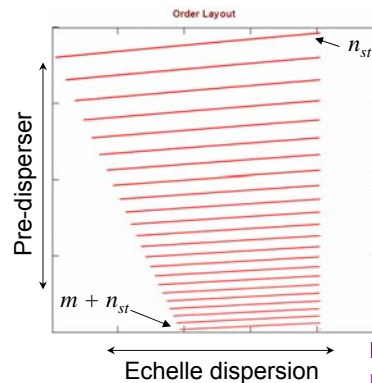
$$\Rightarrow \Delta\lambda = d_g \Delta\beta \cos \beta_1$$

- Where $\Delta\lambda = \lambda / (n_{st} + m)$

$$n_{gap} = \frac{f_{cam} \Delta\beta}{s_{pix}} \quad s_{pix} = \text{pixel size}$$

$$\Rightarrow n_{gap} \sim \frac{\lambda_1}{n_{st} + m} \frac{1}{d_g} \frac{f_{cam}}{s_{pix}} \frac{1}{\cos \beta_1} \quad (\text{pixels})$$

- Slit must be smaller or order overlap occurs



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Echelle Groove Spacing

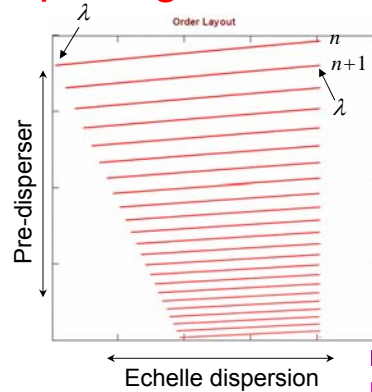
- Using the grating equation for two successive orders at the same wavelength, then differencing gives

$$\begin{aligned} \frac{\lambda}{d_e} &= \sin \beta_{n+1} - \sin \beta_n \\ &= 2 \sin \frac{\beta_{n+1} - \beta_n}{2} \cos \frac{\beta_{n+1} + \beta_n}{2} \end{aligned}$$

- Let ϕ be echelle blaze angle and define: $\beta_1 = \theta_1 + \phi$ and $\beta_2 = \theta_2 + \phi$.
- Taking the lowest order, $\theta_e = \max$ angle of echelle, and $\theta_1 \sim -\theta_2$ then

$$\Rightarrow d_e = \frac{\lambda_2}{2 \cos \phi \sin \theta_e}$$

- Note that $\theta_e \cong \frac{s_{pix} N_{pe}}{2 f_{cam}^\# G_{proj}} = \frac{N_{pe}}{p_{samp} R} \tan \phi$



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Predisperser Groove Spacing

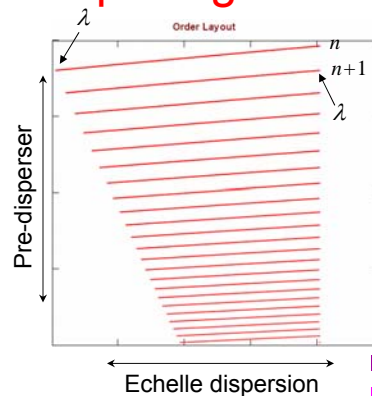
- For 1st order grating predisperser use the grating equation at the ends of the λ range (λ_1, λ_2), then difference

$$\begin{aligned} \frac{\lambda_2 - \lambda_1}{d_g} &= \sin \beta_{2g} - \sin \beta_{1g} \\ &= 2 \sin \frac{\beta_{2g} - \beta_{1g}}{2} \cos \frac{\beta_{2g} + \beta_{1g}}{2} \end{aligned}$$

- Let ϕ_g be grating blaze angle and define: $\beta_{1g} = \theta_{1g} + \phi_g$ and $\beta_{2g} = \theta_{2g} + \phi_g$.
- Taking the lowest order, $\theta_g = \max$ angle of grating, and $\theta_{1g} \sim -\theta_{2g}$ then

$$\Rightarrow d_g = \frac{\lambda_2 - \lambda_1}{2 \cos \phi_g \sin \theta_g}$$

- Note that $\theta_g \cong \frac{s_{pix} N_{pg}}{2 f_{cam}^\# G_{proj}} = \frac{N_{pg}}{p_{samp} R} \tan \phi$



Echelle Gratings

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Example: GEDI Spectrograph

Gemini Exoplanet
Discovery Instrument

- Key Specs
 - $R = \lambda/\Delta\lambda = 25,000$
 - Cover 0.9 – 1.8 μm , simultaneously
- Sampling
 - ~ 3 pixels per spectral resolution element
- Number of input beams
 - 4 = (2 beams of EDI) × (1 source + ref. beam)
- Choices
 - One 2048x2048 focal plane array
 - Cost factor – but there is enough spectral coverage w/ one
 - Cool spectrograph to ~ 180 – 200K
 - To keep spectrograph background << stellar photon rate
 - Fiber feed with surrounding guide fibers
 - Two bundles on sky for source and background

These are not quite
the final design specs.

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Size of Echelle

- As discussed, the spectral resolution drives the size of the echelle. The figure below shows a schematic layout of a system.

$$G_{proj} = \frac{R}{2 \tan \phi} \frac{W}{f_{col}^{\#}} = \frac{R}{2 \tan \phi} \frac{\theta_s D_t}{2063} d_{frd}$$

$R = \lambda/\Delta\lambda$

$D_t = \text{telescope diameter (in m)}$

$d_{frd} = \text{fiber focal ratio degradation}$
 $= 1.064 * 1.048 = 1.12$

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Governing Equations

- With an IFU, the camera f-number ($f_{cam}^{\#}$), the project size of the echelle (G_{proj}), and the array size ($N_{px} \times N_{py}$) are computed as:

$$f_{cam}^{\#} = \frac{s_{pix} P_{samp} f_{ifu}}{\theta_s D_t d_{frd}} \quad G_{proj} = \frac{R}{2 \tan \phi} \frac{\theta_s D_t}{f_{ifu}} d_{frd}$$

$$N_{px} N_{py} \approx n_{spo} P_{samp} (n_{sp} + P_{samp} f_{ifu}^2) \frac{\lambda_2 (\lambda_2 - \lambda_1)}{\lambda_1^2} R$$

- | | |
|---|---|
| s_{pix} = pixel size (= 18 μm) | R = $\lambda/\Delta\lambda$ (= 25,000) |
| P_{samp} = sample per resolution element (~ 3) | ϕ = echelle blaze angle (= 75.96°) |
| f_{ifu} = number of sub-slits (1, 2, 3, ...) | λ_1 = starting λ (= 0.9 μm) |
| D_t = telescope diameter (= 8.1 m) | λ_2 = ending λ (= 1.8 μm) |
| θ_s = slit size on sky (= 1.1") | N_{px} = array cols |
| d_{frd} = fiber focal ratio degradation
= 1.064*1.048 = 1.12 | N_{py} = array rows |
| | n_{spo} = # of spectra per order (= 6) |
| | n_{sp} = gap between spectra (= 2 pix) |

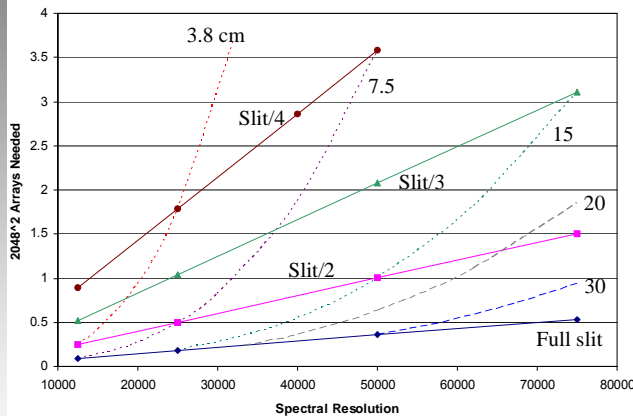
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Spectrograph Design Space w/o EDI



Plot of number of required 2048x2048 arrays versus spectral resolution for 8-m telescope with 1.1" slit. Solid lines represent constant slit size. Dashed lines indicate a fixed projected echelle size (in cm) as indicated.

The slit is made smaller by an IFU which divides the slit and remaps it into the cross-dispersion direction.

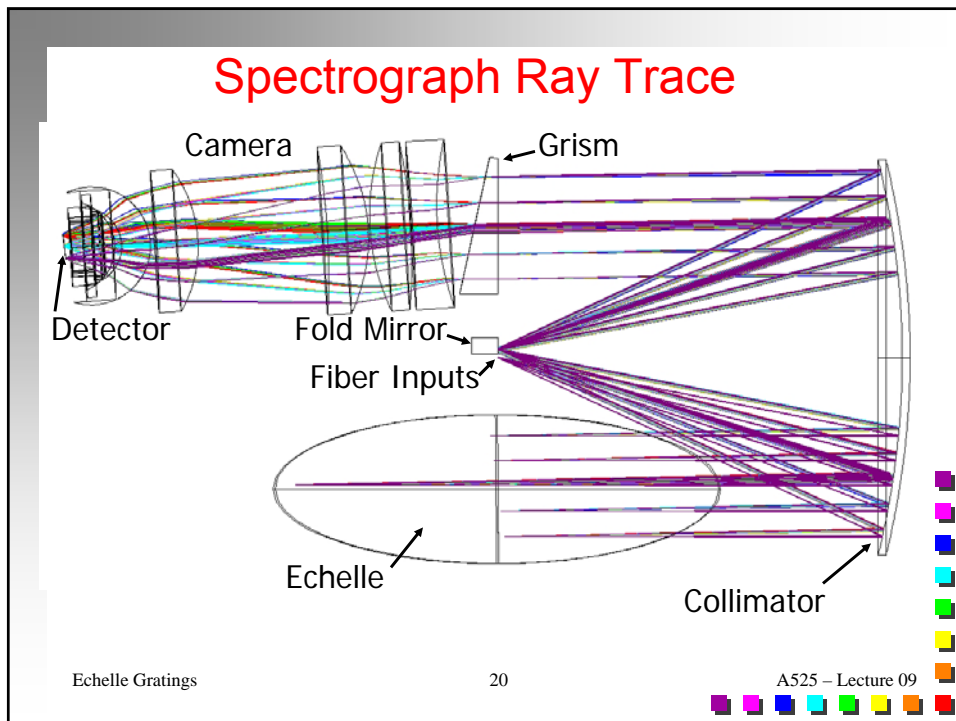
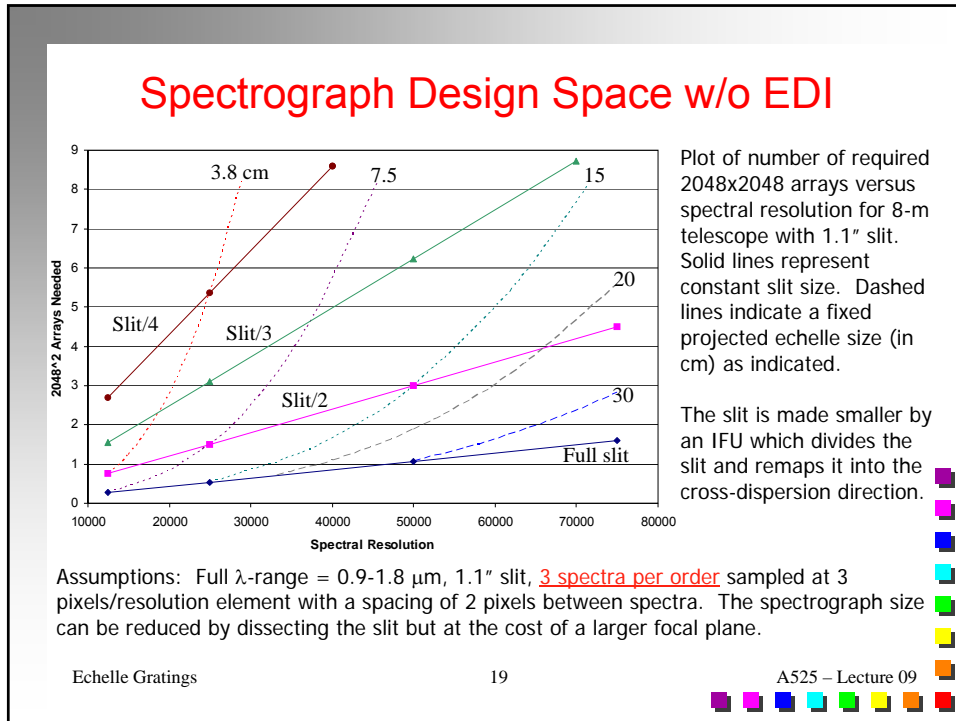
Assumptions: Full λ -range = 0.9-1.8 μm , 1.1" slit, 1 spectra per order sampled at 3 pixels/resolution element with a spacing of 2 pixels between spectra. The spectrograph size can be reduced by dissecting the slit but at the cost of a larger focal plane.

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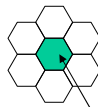
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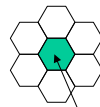


Fiber feed

Layout in telescope focal plane



Source Fiber



Sky Fiber

- Switch between source and sky positions.
- Problem with this design is the we (potentially) get a $\sqrt{2}$ noise increase if we subtract a single background fiber.
- Should we have more sky positions (instead of dark areas) on the array? – no room on array.

Fiber path

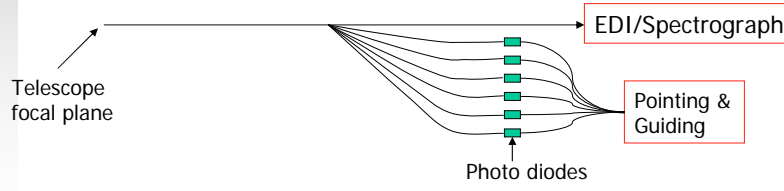


Photo diodes

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Current Design

R ($\lambda/\Delta\lambda$)	Pix/S E	Num. Orders	Sp/ Order	f/#	P (cm)	Gap (pix)	Array Format
25,000	3.0	35	4	1.3	13.3	9	2048x2048
	2.5	29	4	1.1	13.3	14	2048x2048

- Columns are spectral resolution, pixels per resolution element, number of orders, spectra per order, array camera f-number, projected echelle size, gap between spectra, and array format.
- Assumes 1.1" slit. For R = 25,000 the "gap" is computed assuming four spectra per order which are grouped as pairs.

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Spectrum layout options

Option 1:
Equally spaced spectra

Option 2:
Paired spectra

Orders 35 - 75 used

- Accept both output beams from the EDI. Assume each beam has both a stellar spectrum and an emission lamp spectrum
 - Can equally space spectra within an order or
 - Put reference spectrum near stellar spectrum

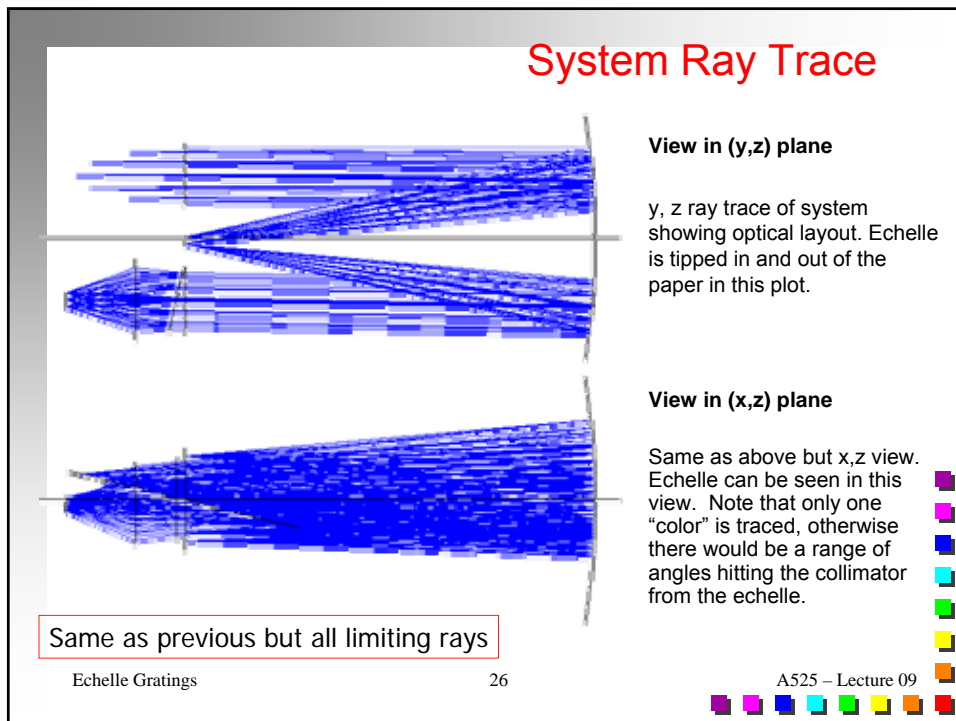
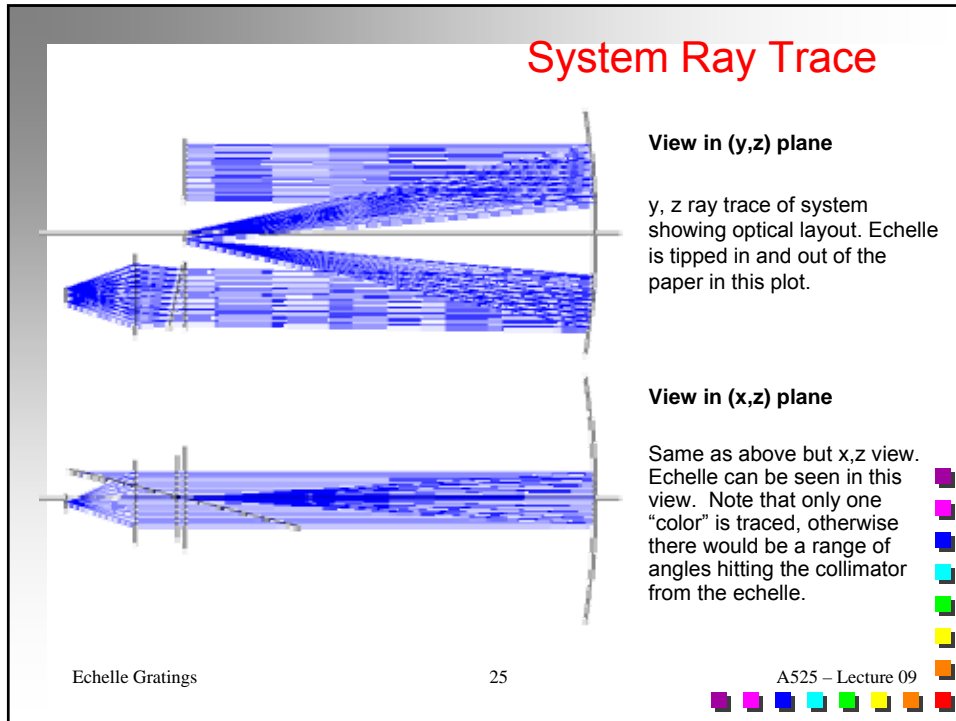
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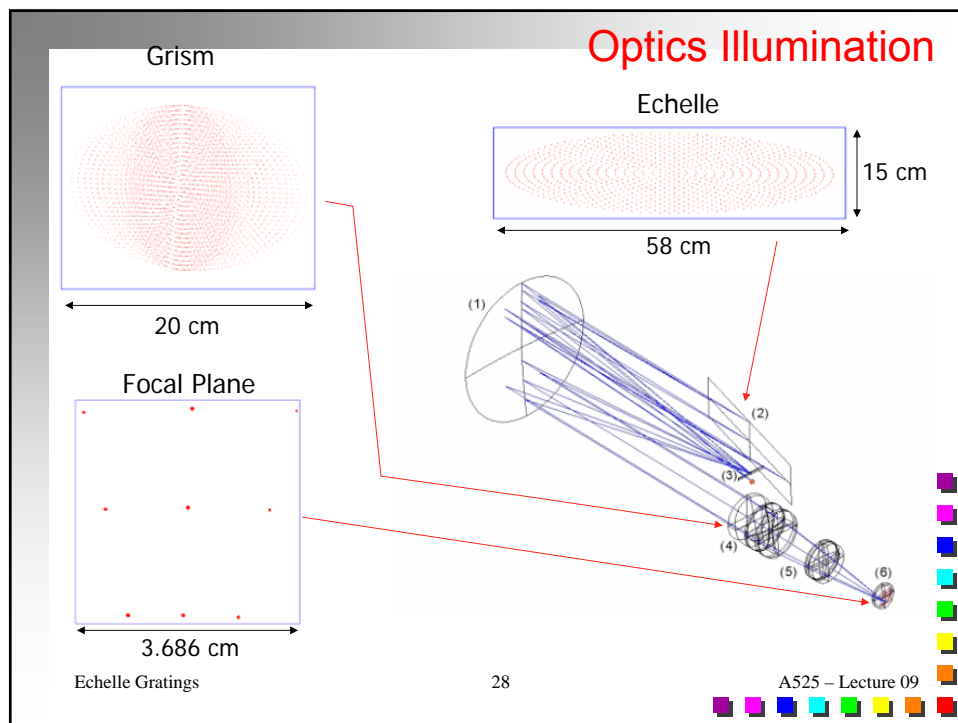
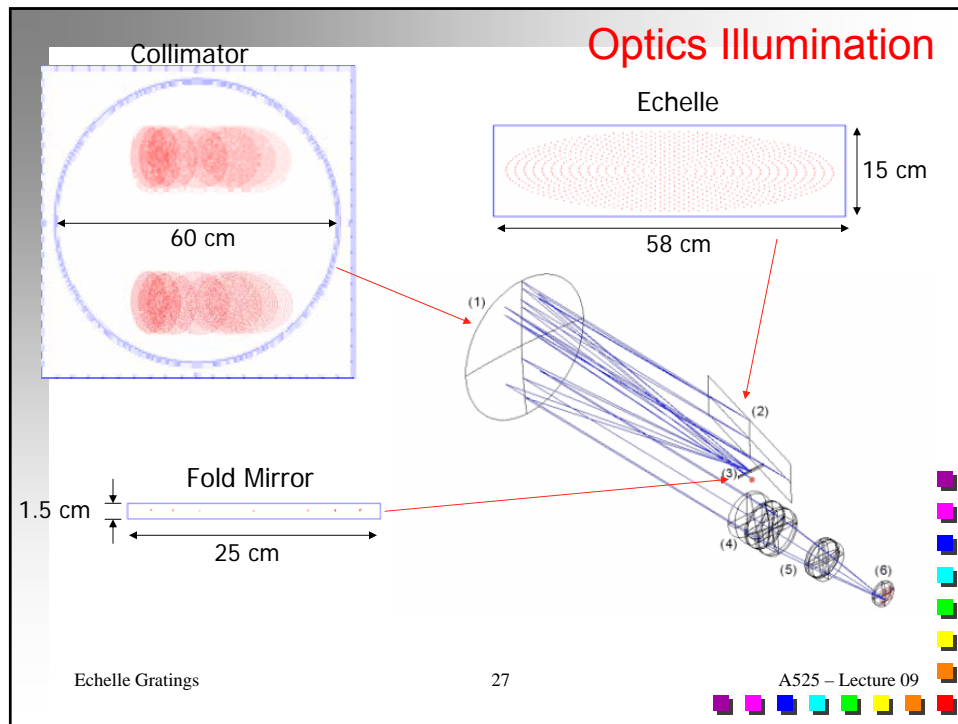
Basic Layout

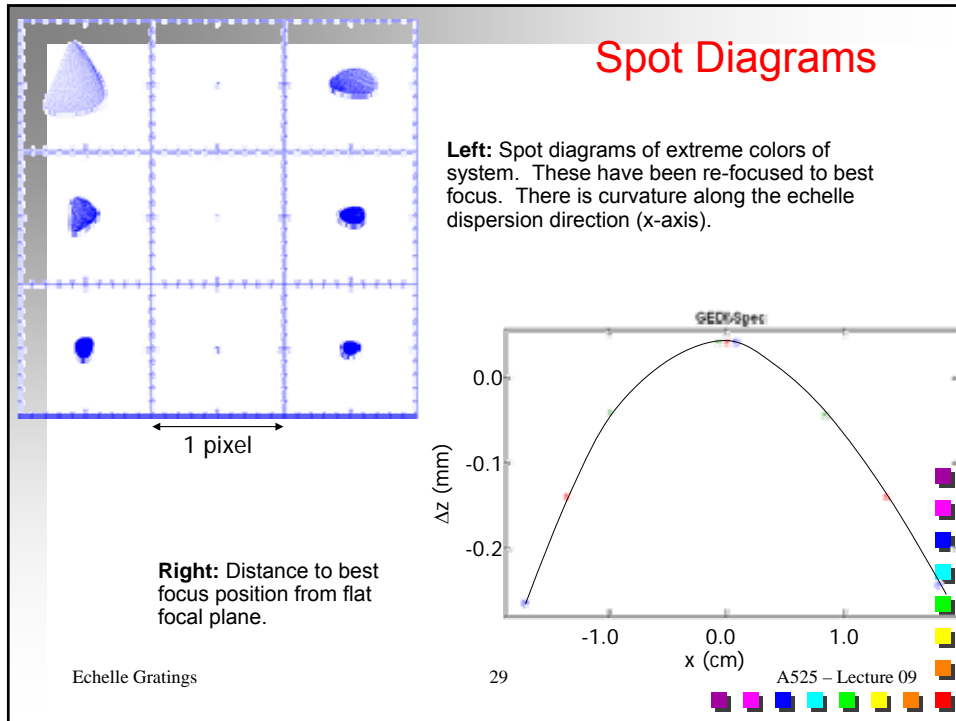
- Optical path is from entrance point (red dot) to f/7.5 collimator, echelle, collimator (now a camera), fold mirror, collimator, grism, f/1.25 camera, and focal plane with a field lens.

- (1) f/7.5 Collimator
- (2) Echelle
- (3) Fold mirror
- (4) Grism
- (5) Camera
- (6) Focal Plane

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GEDI Spectrograph Design Parameters

Echelle:

- Blaze Angle: 75.9638 deg [tan(alpha) = 4]
- Groove Spacing: 35 microns in narrow direction
- Size: 58 x 15 cm
- Operation Orders: 38 – 75
- λ Range: 0.9 – 1.8 microns

Grism:

- Apex Angle: 13.0 deg
- Groove Spacing: 4.5 microns in wide direction
- Index of refraction: 2.4 (KRS5)
- Size: 20 x 16 cm
- Operation Order: 1

Collimator:

- Focal Length: 100 cm (f/7.5)
- Diameter: 60 cm
- x,y position: 0, 0 cm (relative to slit)

Camera:

- Focal Length: 16.875 cm (f/1.25)
- Entrance Diameter: 20 cm
- x,y position: -1, -15.33 cm (relative to slit)

Image Scale:

- Image scale: 1.1 arcsec => 324 micron at entrance to spectrograph
- At focal plane: 53.2 microns = 2.96 pixels (18 microns/pixel)

These are not the final design specs, but are illustrative.

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